Microstructure evolution and mechanical properties of Co-Fe-Ni-Ti-V eutectic high entropy alloy

Rahul M R^{1a}, Reliance Jain^{2a}, Sumanta Samal^{2b*}, Gandham Phanikumar^{1b}

1Department of Metallurgical and Materials Engineering, Indian Institute of Technology Madras, Chennai-600036, Tamil Nadu, India.

²Discipline of Metallurgy Engineering and Materials Science, Indian Institute of TechnologyIndore, Khandwa Road, Simrol, Indore-453552, Madhya Pradesh, India.

^{1a}rahulmr1991@gmail.com, ^{1b}gphani@iitm.ac.in, ^{2a}phd1701105011@iiti.ac.in, ^{2b*}sumanta@iiti.ac.in

ISBN: 978-963-508-889-8 Solidification and Gravity VII Miskolc-Lillafüred, Hungary September 3-6, 2018

Keywords: Eutectic high entropy alloy (EHEA), Microstructure evolution, Phase equilibria, Pseudo-quasiperitectic reaction, Mechanical property.

Abstract:

The present study is aimed at understanding the sequence of phase evolution during solidification in $Co_{25}Fe_{25}Ni_{25}Ti_{20}V_5$ eutectic high entropy alloys (EHEAs), synthesized byvacuum arc melting cum suction casting technique. The detailed X-ray diffraction (XRD) and electron microscopic (SEM and TEM) coupled with energy dispersive spectroscopic (EDS)analyses reveal the presence of BCC (β), FCC_1 (α 1), FCC_2 (α 2) and Ni₃Ti phases. For Co-Fe-Ni-Ti-V HEA, at first Ni₃Ti (DO24) primary dendritic phase is formed from theliquid, followed by peritectic reaction to form FCC_1 (α 1) phase (i.e. Ni₃Ti + L \rightarrow FCC_1(α 1)). Then the remaining liquid undergoes eutectic reaction to form FCC_1 (α 1) and FCC_2 (α 2)phases (i.e. coarse eutectic: L \rightarrow FCC_1 (α 1) + FCC_2 (α 2)). Finally, the remaining liquidundergoes eutectic reaction to form BCC (β), and FCC_2 (α 2) (i.e. fineeutectic: L \rightarrow BCC (β) + FCC_2 (α 2). Therefore, based upon sequence of microstructural evolution, two pseudo-quasiperitectic reactions i.e. L+Ni₃Ti \rightarrow FCC_1 (α 1) + FCC_2 (α 2) and L+ FCC_1 (α 1) \rightarrow BCC (β) + FCC_2 (α 2) have been proposed for the investigated EHEA. It is also found that Co₂₅Fe₂₅Ni₂₅Ti₂₀V₅EHEAs retains high strength at elevated temperature.

1. Introduction

The complex concentrated high entropy alloys (HEAs) [1-8] consisting multiple principal elements in equiatomic or near equiatomic ratio exhibits simple microstructure of FCC and/or BCC solid solution phase. This is attributed to the several important ore effects in HEAs [4, 5] such as high configurational entropy, severe lattice distortion and sluggish diffusion [9, 10]. Yeh et al. [1] first reported CuCoNiCrAl_xFe HEAs which shows good strength at elevated temperature up to 500°C. The refractory HEAs such as Nb₂₅Mo₂₅Ta₂₅W₂₅

and $V_{20}Nb_{20}Mo_{20}Ta_{20}W_{20}$ alloys have been studied by Senkov et al. [11] which exhibits excellent mechanical properties at high temperatures. Similarly, new class ofmulticomponent eutectic HEAs[5, 12-14], exhibiting good high temperature strengthhave also been reported in the open literature. Although a lot of new and exciting research work has been done by many research groups across globe in the field of HEAs to designnovel materials for possible industrial applications by choosing elements and composition judiciously in order to obtain unique microstructural features. Therefore, an attempt is made in this direction to develop novel HEA with improved mechanical properties at elevated temperature.

The objective of the present study is to understand the sequence of phase evolution during solidification and to establish new phase equilibria based upon detailed microstructural characterization as well as to evaluate the high temperature mechanical properties in the newly designed multicomponent $Co_{25}Fe_{25}Ni_{25}Ti_{20}V_5$ HEA.

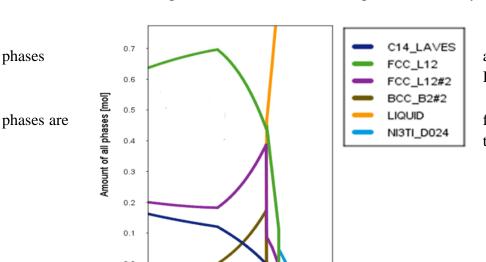
2. Experimental materials and procedures

High purity commercial Co, Fe, Ni, Ti and Velementswere used as the starting materials to prepare $Co_{25}Fe_{25}Ni_{25}Ti_{20}V_5$ HEA (henceforth referred to as EHEA) by arc melting technique under ultra high purity argon gas to obtain arc melted alloy button. The structural characterization of studied high entropy alloy was carried by X-ray diffraction (XRD) (Panalytical X-pert pro instrument) with Cu- K_{α} ($\lambda=0.154056$ nm) radiation, operating at 45 kV and 30 mA, with step size of $2\theta=0.017$ deg. The peaks in the XRD pattern were identified using International Committee for Diffraction Data (ICDD) database in PCPDFWIN software. The microstructural characterization of the samples was examined using the scanning electron microscope (Inspect F) equipped with an energy-dispersive spectrometer (EDS). Isothermal hot compression tests of the cylindrical samples ($\phi=6$ mm and aspect ratio of 1.5:1) were carried out using Gleeble 3800® thermo mechanical simulator at deformation temperatures of 800°C (1073 K) and 1000°C (1273 K) with constant strain rates of 10^{-1} .

3. Results and Discussion

3.1. Thermodynamic simulation

The thermodynamic simulations (as shown in Figure 1) of studied multicomponent EHEA have been carried out to understand the phase evolution and predict the equilibrium solidification path using TCHEA database in ThermoCalc software.It is observed that there are six equilibrium phases such as Ni₃Ti_DO24, FCC_L12, FCC_L12≠2, BCC_B2≠2, C14_LAVES and LIQUID phases from liquidus temperature (~1101°C) to 780°C. It is to be noted that at first Ni₃Ti phase is formed from the liquid, followed by formation of both



1050 1100 1150 1200 1250 1300 1350 1400 1450

Temperature [K]

FCC_L12, FCC_L12 \neq 2 and finally BCC_B2 \neq 2 and C14_LAVES formed in this temperature range.

Figure 1: Thermodynamic simulation of multicomponent Co₂₅Fe₂₅Ni₂₅Ti₂₀V₅HEA.

3.2. Structural characterization

The XRD pattern of multicomponent EHEA is shown in Figure 2a. The XRD pattern shows the intense diffraction peaks corresponding to BCC solid solution phase (β), Disorder FCC1 solid solution phase (α 1), Order FCC2(L12) solid solution phase (α 2) and ordered Ni₃Ti DO24.

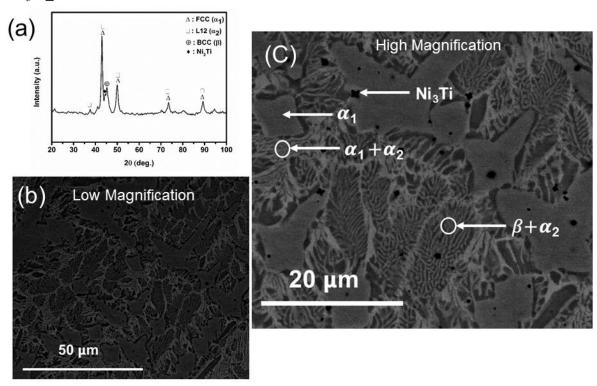


Figure 2: (a) XRD pattern, (b) and (c) SEM micrograph of multicomponent $Co_{25}Fe_{25}Ni_{25}Ti_{20}V_5HEA$.

3.3. Microstructural characterization

The detailed microstructural characterization of multicomponent EHEA was carried out using back scattered electron (BSE) imaging mode in SEM. However, the representative SEM micrograph of the studied HEA is given in Figure 2b(low magnification image) and Figure 2c (high magnification image) to decipher the different phases in the microstructure. The different phases in the microstructure of the studied HEA are marked based on the compositional analyses using SEM coupled with EDS. The compositional measurement of

each phases in microstructure has also been carried out using TEM coupled with EDS (as shown in Table 1).

Phases	Co	Fe	Ni	Ti	V
$FCC(\boldsymbol{\alpha}_{l})$	24.20	24.30	22.20	24.40	4.90
$FCC(\boldsymbol{\alpha}_2)$	25.10	25.70	20.60	24.50	4.10
BCC (B)	29.90	30.60	9.90	23.80	5.90
Ni ₃ Ti	23.59	22.03	26.97	22.05	5.36

Table 1: EDS analysis of all the phases (composition in atomic percent) in microstructure of multicomponent $Co_{25}Fe_{25}Ni_{25}Ti_{20}V_5$ HEA.

The microstructure of multicomponentEHEA reveals the presence of primary $(Ni,Fe,Co)_3$ Tiwith black contrast, Ni-rich (i.e. Ni-Co-rich phase) solid solution phase with bright contrast (α_1) as well as light contrast (α_2) andNi-lean (i.e. Fe-Co-rich phase) solid solution phase gray contrast (β) .

A detailed TEM characterization of the suction cast ($\phi = 6$ mm) EHEAwas done to elucidate the fine scale microstructural features (shown in Figure 3). The phases in the microstructure are identified using the obtained selected area diffraction (SAD) patterns. The microstructure reveals the presence of two eutectics i.e. (i) one eutectic is between disorder FCC1 solid solution phase (α_1) and order FCC2 solid solution phase (α_2) and (ii) other one is between order FCC2 solid solution phase (α_2) and BCC (β) solid solution phase as well as two dendritic phases i.e. ordered Ni₃Ti_DO24 and disorder FCC1 solid solution phase (α_1). It is important to note that all the equilibrium phases predicted by thermodynamic simulation (Figure 1) except C14_LAVES phase are observed in the microstructure of the studied EHEA.

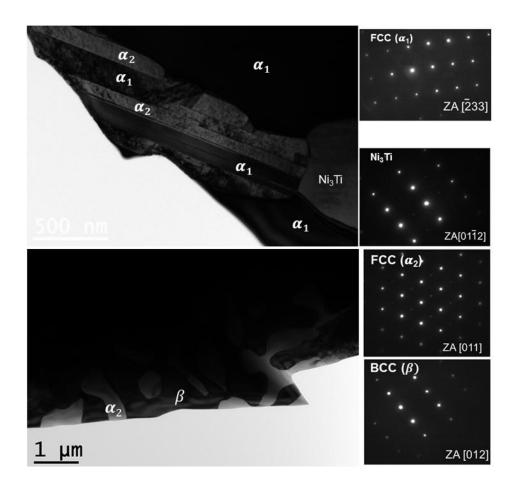


Figure 3: TEM micrograph of multicomponent Co₂₅Fe₂₅Ni₂₅Ti₂₀V₅HEA.

3.4. Phase equilibria in multicomponent Co₂₅Fe₂₅Ni₂₅Ti₂₀V₅HEA

It is important to note from microstructural characterization that there are one peritecticreaction i.e. Ni₃Ti + L \rightarrow FCC_1(α ₁) and two eutectics reactions i.e.coarse eutectic: L \rightarrow disorder FCC_1 (α ₁) + order FCC_2 (α ₂) and fineeutectic: L \rightarrow order FCC_2 (α ₂) + BCC (β) features in the microstructure of studied HEA.

The solidification pathways for the investigated multicomponent EHEA has been described in the following;

- (i) at first Ni₃Ti primary dendritic phase is evolved from the liquid during solidification, followed by
- (ii) the peritectic reaction to form disorder FCC_1 solid solution phase FCC_1(α_1) i.e. Ni₃Ti + L \rightarrow FCC 1(α_1)and then
- (iii) the remaining liquid undergoes eutectic reaction to from disorder FCC_1 (α_1) and order FCC_2 (α_2)phases (i.e. coarse eutectic: L \rightarrow FCC_1 (α_1) + FCC_2 (α_2)and
- (iv) finally, the remaining liquidundergoes eutectic reaction to form order FCC_2 (α 2) and BCC (β) (i.e. fineeutectic: L \rightarrow FCC_2 (α 2) + BCC (β)

Based upon the microstructural features observed in the studied multicomponent EHEA, the two different types of four phases reactions i.e. L+ Ni₃Ti \rightarrow FCC_1 (α_1) + FCC_2 (α_2) and L+ FCC_1 (α_1) \rightarrow FCC_2 (α_2) + BCC (β) have been proposed for the investigated HEA. These four phase reactions are known as pseudo-quasiperitectic reactions. The first four phases reaction at point P1 is cooperated by two reactions i.e. Ni₃Ti + L \rightarrow FCC_1(α_1) and L \rightarrow FCC_1 (α_1) + FCC_2 (α_2) above and below point P1 respectively. Similarly, thesecond four phases reaction at point P2 is cooperated by two eutectic reactions i.e. L \rightarrow FCC_1 (α_1) + FCC_2 (α_2) and L \rightarrow FCC_2 (α_2) + BCC (β) above and below point P2 respectively.

3.5. Mechanical properties of Co₂₅Fe₂₅Ni₂₅Ti₂₀V₅HEA

The true stress-strain curves of the multicomponent EHEAat different temperatures (700°C (973 K), (800°C (1073 K), (900°C (1173 K) and 1000°C (1273 K) at a fixed strain rate of 10^{-1} s⁻¹ were obtained for cylindrical samples (diameter (ϕ) = 6 mm and aspect ratio of 1.5:1). It is to be noted from Figure 4 that the flow stress decreases with increase in temperature at a constant strain rate of 10^{-1} s⁻¹.

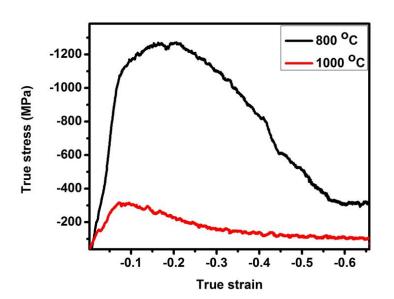


Figure 4:(a) True stress vs. strain curve of the multicomponent $Co_{25}Fe_{25}Ni_{25}Ti_{20}V_5HEA$ at $800^{\circ}C$, $1000^{\circ}C$ and strain rate of 10^{-1} s⁻¹.

It is also observed that after the reaching the yield stress, the studied alloy deforms plastically up to 65 % of true strain value with no fracture of the specimen. It is important to note that the high strength of the studied HEA at high temperature is attributed to the presence of unique composite microstructure i.e. bimodal eutectics at different length scale and peritectic morphology. One major finding of the present study is the presence of two different eutectics at different length scale in the designed multicomponent HEAs. Therefore, this type of unique microstructural features consisting of peritectic and bimodal eutecticsat different length scale observed in the studied multicomponent EHEA can be considered as potential candidate for high temperature structural applications.

4. Conclusions

Based on the results and discussion with respect to the present investigated multicomponentCo₂₅Fe₂₅Ni₂₅Ti₂₀V₅HEA, the following conclusion can be drawn;

- The detailed sequence of phase evolution in the newly designed multicomponent HEAhas been understood by adopting experimental and thermodynamic simulation approach.
- The new phase equilibria i.e. Pseudo-quasiperitectic reactions have been proposed in the designed multicomponent HEA
- The high strength at elevated temperature is attributed to the unique microstructural features consisting of one peritectic and two types of eutectics in the microstructure.

References:

- [1] J.W. Yeh, S.K. Chen, S.J. Lin, J.-Y. Gan, T.S. Chin, T.T. Shun, C.H. Tsau, S.Y. Chang, Adv. Eng. Mater. 6 (2004) 299–303.
- [2] B. Cantor, I.T.H. Chang, P. Knight, A.J.B. Vincent, Mater. Sci. Eng. A. 375-377 (2004) 213–218.
- [3] S. Mridha, S. Samal, P.Y. Khan, K. Biswas, Govind, Metall. Mater. Trans. A Phys. Metall. Mater. Sci. 44 (2013) 4532–4541.
- [4] B.S. Murty, J.W. Yeh, S. Ranganthan, High Entropy Alloys, Elsevier, 2014.
- [5] S. Guo, C. Ng, C.T. Liu, Mater. Res. Lett. 1 (2013) 228–232.
- [6] Y. Zhang, T.T. Zuo, Z. Tang, M.C. Gao, K. A. Dahmen, P.K. Liaw, et al., Prog. Mater. Sci. 61 (2014) 1–93.
- [7] S. Samal, S. Mohanty, A.K. Misra, K. Biswas, B. Govind, Mater. Sci. Forum. 790-791 (2014) 503–508.

- [8] S. Mohanty, S. Samal, A. Tazuddin, C.S. Tiwary, N.P. Gurao, K. Biswas, Mater. Sci. Technol. 31 (2015) 1214–1222.
- [9] K.Y. Tsai, M.H. Tsai, J.W. Yeh, Acta Mater. 61 (2013) 4887–4897.
- [10] D.L. Beke, G. Erdélyi, Mater. Lett. 164 (2016) 111–113.
- [11] O.N. Senkov, G.B. Wilks, J.M. Scott, D.B. Miracle, Intermetallics. 19 (2011) 698–706.
- [12] A.K. Mishra, S. Samal, K. Biswas, Trans. Indian Inst. Met. 65 (2012) 725–730.
- [13] S. Samal, Rahul MR, R. S. Kottada, G. Phanikumar, Mater. Sci. Eng. A, 664 (2016) 227–235, 2016.
- [14]Rahul MR, S. Samal, S. Venugopal, G. Phanikumar, J. Alloys Compd., 749 (2018) 1115-1127